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TRANSMITTAL FORM (to be used for correspondence after initial filing) DEC 11 2003 PATENT & TRADEMARK OFFICE	Application Number	09/837,974
	Filing Date	04/19/2001
	First Named Inventor	Hiroshi Horie et al.
	Group Art Unit	3682
	Examiner Name	J. Stefanon
Total Number of Pages in this Submission	Attorney Docket Number	TWA26USA

ENCLOSURES (check all that apply)

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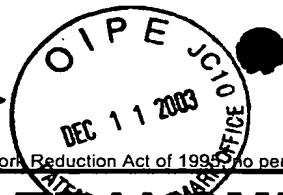
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FEE TRANSMITTAL for FY 2004

Effective 10/01/2003. Patent fees are subject to annual revision.

☐ Applicant claims small entity status. See 37 CFR 1.27

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Complete if Known

Application Number 09/837,974
Filing Date 04/19/2001
First Named Inventor Hiroshi Horie et al.
Examiner Name J. Stefanon
Art Unit 3682
Attorney Docket No. TWA26USA

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GROUP 360

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1. BASIC FILING FEE

Large Entity Fee Code (\$)	Small Entity Fee Code (\$)	Fee Description	Fee Paid
1001 770	2001 385	Utility filing fee	
1002 340	2002 170	Design filing fee	
1003 530	2003 265	Plant filing fee	
1004 770	2004 385	Reissue filing fee	
1005 160	2005 80	Provisional filing fee	
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Total Claims	Extra Claims	Fee from below	Fee Paid
Independent	-20** =	X	
Multiple Dependent	-3** =	X	

Large Entity Fee Code (\$)	Small Entity Fee Code (\$)	Fee Description
1202 18	2202 9	Claims in excess of 20
1201 86	2201 43	Independent claims in excess of 3
1203 290	2203 145	Multiple dependent claim, if not paid
1204 86	2204 43	** Reissue independent claims over original patent
1205 18	2205 9	** Reissue claims in excess of 20 and over original patent

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1051 130	2051 65	Surcharge - late filing fee or oath	
1052 50	2052 25	Surcharge - late provisional filing fee or cover sheet	
1053 130	1053 130	Non-English specification	
1812 2,520	1812 2,520	For filing a request for <i>ex parte</i> reexamination	
1804 920*	1804 920*	Requesting publication of SIR prior to Examiner action	
1805 1,840*	1805 1,840*	Requesting publication of SIR after Examiner action	
1251 110	2251 55	Extension for reply within first month	
1252 420	2252 210	Extension for reply within second month	
1253 950	2253 475	Extension for reply within third month	
1254 1,480	2254 740	Extension for reply within fourth month	
1255 2,010	2255 1,005	Extension for reply within fifth month	
1401 330	2401 165	Notice of Appeal	
1402 330	2402 165	Filing a brief in support of an appeal	330.00
1403 290	2403 145	Request for oral hearing	
1451 1,510	1451 1,510	Petition to institute a public use proceeding	
1452 110	2452 55	Petition to revive - unavoidable	
1453 1,330	2453 665	Petition to revive - unintentional	
1501 1,330	2501 665	Utility issue fee (or reissue)	
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1503 640	2503 320	Plant issue fee	
1460 130	1460 130	Petitions to the Commissioner	
1807 50	1807 50	Processing fee under 37 CFR 1.17(q)	
1806 180	1806 180	Submission of Information Disclosure Stmt	
8021 40	8021 40	Recording each patent assignment per property (times number of properties)	
1809 770	2809 385	Filing a submission after final rejection (37 CFR 1.129(a))	
1810 770	2810 385	For each additional invention to be examined (37 CFR 1.129(b))	
1801 770	2801 385	Request for Continued Examination (RCE)	
1802 900	1802 900	Request for expedited examination of a design application	

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SUBTOTAL (3) (\$ 330.00)

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(Attorney/Agent)

24,442

(Complete if applicable)

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12/9/03

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#14/Appeal
Brief
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IN THE UNITED STATES PATENT AND TRADEMARK OFFICE **RECEIVED**
DEC 16 2003

In re the Application of
H. Horie et al.

Serial No.: 09/837974

Filed: April 19, 2001

For: SILENT CHAIN
POWER TRANSMISSION APPARATUS

Examiner:
J. Stefanon

Art Unit: 3682

GROUP 3600

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BRIEF ON APPEAL

(1) Real party in interest

The real party in interest is the Applicants' assignee, Tsubakimoto Chain Co., a Japanese corporation located at Osaka Fukokuseimei Building 2-4, Komatsubara-cho, Kita-ku, Osaka 530-0018, Japan.

(2) Related appeals and interferences

None.

(3) Status of claims

The pending claims are claims 1 and 2. Both claims are rejected and the rejection of both claims is the subject of this appeal. Claim 3 has been canceled.

(4) Status of Amendments

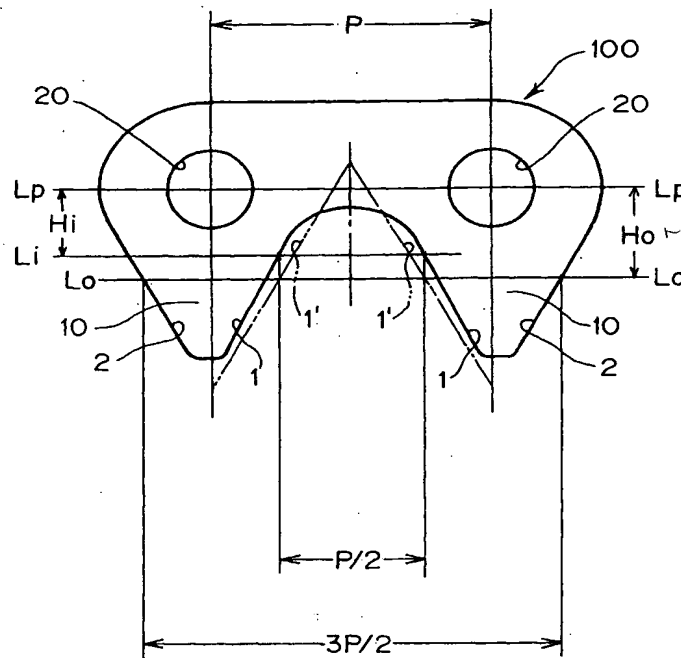
There are no outstanding amendments.

(5) Summary of Invention

A silent chain, also known as an inverted tooth chain, is composed of interleaved W-shaped link plates, as shown in FIG. 7, each plate having a pair of pin holes for receiving

interconnecting pins, and a pair of teeth for engagement with a sprocket.

FIG.7
(Prior Art)



In a typical power transmission application, such as the valve timing system of an automobile engine, the silent chain meshes with sprockets formed by hobbing. (Spec., page 1, lines 5-7; page 2, lines 10-12)

The pitch P of the link plate is the distance between the centers of the pin holes 20, measured along a center line L_p . In the typical silent chain, the inside flanks 1 are located outward relative to imaginary lines 1', which are symmetrical with the outer flanks 2. The inside flanks are always overlapped by the outside flank of an adjacent link plate, and only the outside flanks 2 of the link plates engage the sprocket teeth. As a result, the inside pitch line L_i , which is the line, parallel to the pin center line L_p , and

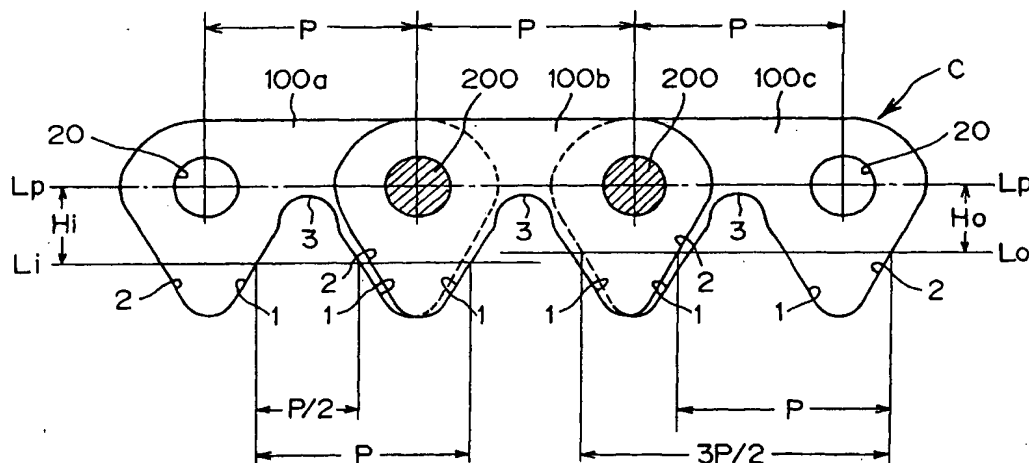
intersecting the inner flanks at a location where the distance between the inner flanks is equal to $P/2$, is relatively close to the center line L_p , compared to the outside pitch line L_o , which is the line intersecting the outer flanks at a location where the distance between the outer flanks is $3P/2$. The distance between the center line L_p and the inside pitch line may be defined as H_i , and the distance between the center line L_p and the outside pitch line may be defined as H_o . In the conventional silent chain, H_i is always less than or equal to H_o ($H_i \leq H_o$). (Spec., pages 1-2)

In the conventional chain transmission, as the sprocket rotates through an angle $\alpha/2$ (α being the sprocket pitch angle), from the position shown in FIG. 8 to the position shown in FIG. 9, the center of pin 200a moves downward through a distance $H_s = U - V$, where $U = \frac{P}{2\sin(\frac{\alpha}{2})}$ and $V = \frac{P}{2\tan(\frac{\alpha}{2})}$. As a

result of this motion, known as "polygonal motion," the free span of the conventional chain moves in the up and down direction as it approaches the sprocket. This up and down motion of the free span of the chain causes undesirable vibration and impact noise, and shortens the life of the chain. (Spec., page 2, line 17, page 4, line 6)

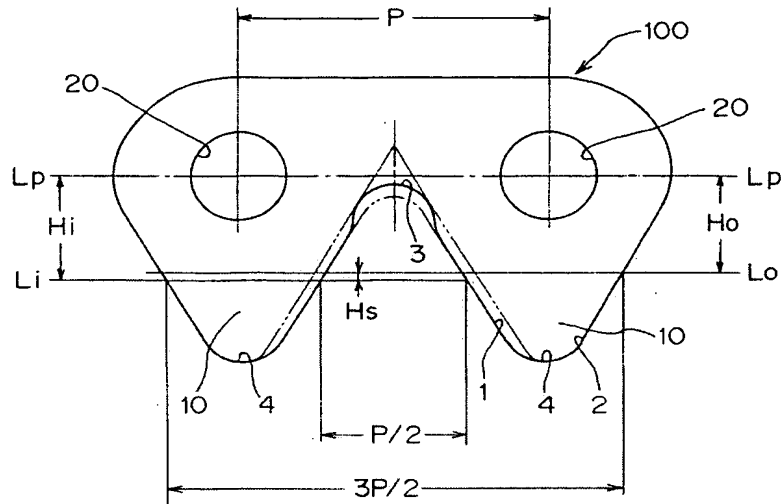
One attempt at solving the problem of up and down motion was to form the sprocket using a rack cutter, so that its tooth profiles were identical to the profiles of the link plates when the chain is stretched linearly. However, this measure afforded only a partial solution to the problem of up and down movement of the chain. (Spec., page 4, line 7 - page 5, line 7.)

FIG. 1



¹In FIG. 2, the outer pitch distance, $3P/2$, is erroneously illustrated. Both limits should have extended to the outside pitch line L_o .

FIG.2



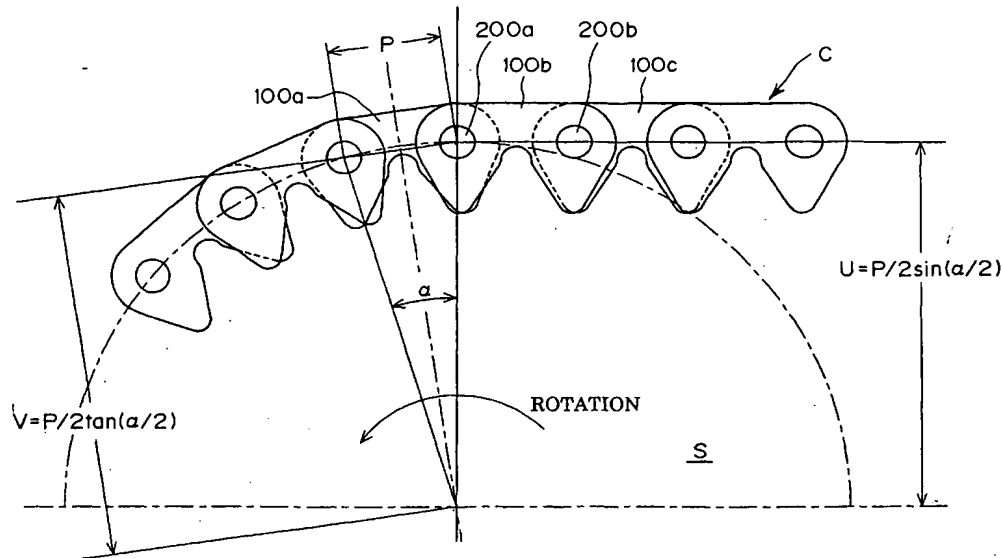
In addition, when the chain is straight, the tooth faces of the links of the chain conform to the profiles of axially, linearly arranged teeth of the hob cutter used to form the teeth of the sprocket. (Spec., page 15, lines 12-14).

Moreover, as shown in FIGs. 1, 2 and 6, the concave bottom surface of the link plate is scooped out more deeply than an arc tangent to the inside tooth faces. (Spec., page 14, lines 6-15).

In the operation of the invention, since the distance H_i , from the inside pitch line L_i to the pin center line L_p , is greater than the distance H_o , from the outside pitch line L_o to the pin center line L_p , by an amount corresponding to the amplitude H_s of polygonal motion of the chain on the sprocket, that is, $H_i = H_o + H_s$, the leading inside tooth face of each link plate is held against a mating sprocket tooth as the link plate meshes with the sprocket. As a result, the link plates remain constantly at the height U during the initial part of the meshing engagement. For example, the leading inside tooth face of link plate 100c, as shown in FIG. 4, engages a sprocket tooth, and this engagement keeps the link plate 100c

at a constant height U as its pin 200b arrives at the position where pin 200a was.

FIG. 4



The leading inside tooth faces move away from the sprocket teeth as the chain bends around the sprocket (page 17, lines 26 - 27), and polygonal motion commences as the link plates become seated on the sprocket with their outer tooth faces in engagement with the sprocket teeth. However, as shown in FIG. 6, where the link plate is shown with one of its outer tooth faces engaged with a sprocket tooth, even though the inside tooth faces conform to the shape of the hob teeth used to make the sprocket, the scooped out bottom surface 3 of the link plate prevents the polygonal motion, which has an amplitude H_s , from resulting in interference between the sprocket teeth and the concave bottom surfaces of the link plates. (Spec., page 18, line 10 - page 19, line 14)

(6) Issues

Page 7 of 14

(7) Grouping of Claims

Claims 1 and 2 are grouped together; no separate reason is presented in support of claim 2.

(8) Argument

"In holding an invention obvious in view of a combination of references, there must be some suggestion, motivation, or teaching in the prior art that would have led a person of ordinary skill in the art to select the references and combine them in the way that would produce the claimed invention. . . . It is insufficient that the prior art disclosed the components of the patented device, either separately, or used in other combinations; there must be some teaching, suggestion, or incentive to make the combination made by the inventor."

Karsten Manufacturing Corp. v. Cleveland Golf Co., 1242 F3d 1376, 58 USPQ2d 1286 (Fed. Cir. 2001).

The final rejection is under 35 USC §103, and based upon a combination of three references, U.S. patents 3,661,025 (Avramidis) and 5,628,702 (Kotera), and Japanese Doc. No. 2000-65156 (Matsuda)².

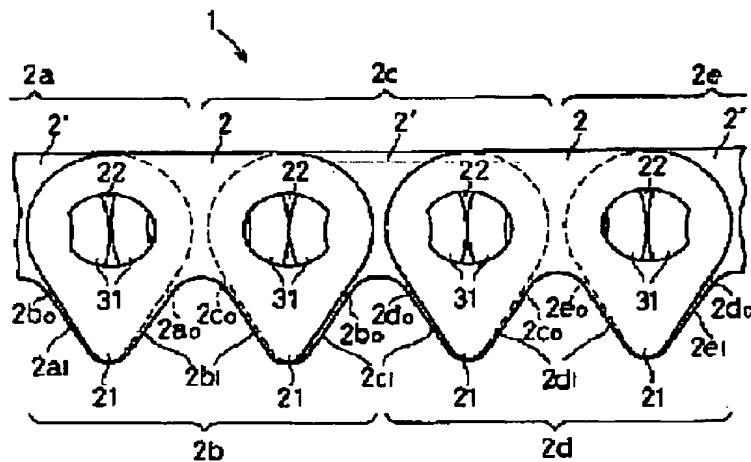
Avramidis relates primarily to a bushing structure in a silent chain, but discloses a silent chain having links with steep outer tooth faces, and inner tooth faces which are much less steep than the outer tooth faces. The inner tooth faces are connected by a scooped-out arc, apparently to provide clearance for the sprocket teeth.

Kotera describes a silent chain in which the inside flanks of the link plates are convex and protrude beyond the outside flanks of adjoining link plates so that the inside flanks of the links contact the sprocket teeth first at the beginning of engagement of the sprocket, thereby pushing up the chord of the chain and reducing chordal motion. The link

²For convenience, U.S. patent 6,244,983 may be referred to as an English language counterpart to the cited Japanese document.

plates then become seated on the sprocket with their outside flanks contacting the sprocket teeth. (Kotera col. 2, lines 31-39) As the Examiner has pointed out, this structure inherently provides a pitch line relationship in which the distance between the pin center line and the inner tooth pitch line is greater than the distance between the pitch center line and the outer tooth pitch line by a constant amount. That is $H_i = H_o + K$.

In Matsuda, a silent chain is designed so that the engaging point between the link and the sprocket is always on the inner link flank from initial engagement to full engagement (U.S. patent 6,244,983, col. 2, lines 49-51). As seen in FIG. 3, the inner flank has a shape that does not conform to the sprocket tooth. As shown in FIGs. 9-12, the inner flank of the link plate progressively rolls on the sprocket tooth, and is ultimately engaged with the tip portion of the sprocket tooth. At column 1, lines 43 - 50, by way of background, Matsuda mentions an earlier proposal in which the flank side on each link series which engages with a sprocket when the silent chain is extended in a linear form has the same shape as the part of the tooth shape for a rack cutter capable of generating the sprocket. The earlier proposal is depicted in the following drawing from Japanese published application Hei 8-184,348:



(DRAWING FROM HEI 8-184,348)

The reasoning underlying the Examiner's rejection is essentially that Avramidis discloses a chain having the arc-shaped scoop; Kotera discloses the pitch line relationship $H_i = H_o + K$ (K being positive); it would have been obvious to modify the chain of Avramidis so that it has the pitch line relationship taught by Kotera, and to make K equal to the amplitude H_s of the chain's polygonal motion; and to make the inside tooth faces with the same shape as that of a rack cutter capable of generating the sprocket as taught by Matsuda (by Matsuda's reference to Hei 8-184,348).

The errors in the rejection are that the conclusion of obviousness is not based on a suggestion or teaching in the references, and that the rejection does not properly establish obviousness of the Applicants' invention as a whole, as required by 35 USC §103.

In Avramidis' chain, the inside tooth faces have a slope that is much more gradual than that of the outside tooth faces, and the outside tooth faces project far beyond the inside tooth faces when the chain is straight. The inside tooth faces clearly do not contact the sprocket, not even upon

commencement of engagement. The scooped out arc appears to be necessitated by the very gradual slope of the inside tooth faces. If they were connected by an arc tangent to the tooth faces, the arc would interfere with the sprocket teeth.

On the other hand it may be readily seen that, if the inner flanks of one of Avramidis' link plates are brought toward each other to make the chain more like that of Kotera, the scooped out arcs become tangent to the inner tooth faces, and there is no longer "an arc-shaped surface scooped out more deeply than an arc tangent to said opposed inside tooth faces" as set forth in Applicants' claim 1. The result would not correspond to the claimed subject matter taken "as a whole."

Kotera and Matsuda both lack such arc-shaped surface, and apparently there was no perception in either case that a scooped-out arc would be either necessary or desirable in a chain in which the inner tooth faces project beyond the outer tooth faces when the chain is straight.

It follows that, while the prior art documents individually disclose elements of claimed combination, they lack any teaching, suggestion or incentive to make the claimed combination. Kotera and Matsuda do not themselves suggest the scooped-out arc, nor do they disclose any need for the same. Moreover, if Avramidis were modified in accordance with Kotera, or in accordance with Kotera and Matsuda, the scooped out arcs would disappear; the result would not correspond to the Applicant's claims.

(9) Conclusion

For the reasons set forth above, we respectfully submit that the final rejection was in error and should be reversed.

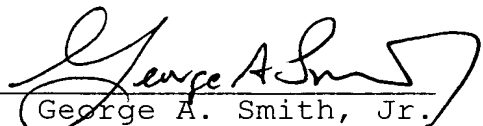
(10) Fees and enclosures

Our check for the fee for filing a brief on appeal, under 37 C.F.R. §1.17(c) is enclosed. If the check is missing or

insufficient, please charge the fee to our deposit account 08-3040.

Two additional copies of this brief are also enclosed.

Respectfully submitted,
HOWSON & HOWSON

By 
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Enclosures:

- (a) 2 additional copies of this brief
- (b) appeal fee

APPENDIX

LISTING OF CLAIMS

1(Previously presented). A silent chain power transmission apparatus comprising:

an endless silent chain comprising a multiplicity of link plates connected in interleaved relationship by a multiplicity of connecting pins, each of said link plates having a pair of V-shaped teeth and a pair of pinholes for fitting said connecting pins, the V-shaped teeth of each said pair having opposed inside tooth faces defining insides thereof and outside tooth faces defining outsides thereof; and

a sprocket having a plurality of teeth in intermeshing relationship with said V-shaped teeth of said link plates;

said inside and outside tooth faces being positioned to satisfy the expression $H_i = H_o + H_s$, where H_i is the distance from a pin center line, passing through the centers of a pair of said connecting pins, to a pitch line of the inside tooth faces of a link plate in which said pair of connecting pins is fitted, H_o is a distance from said pin center line to a pitch line of the outside tooth faces of a link plate in which said pair of connecting pins is fitted, and H_s is the amplitude of polygonal motion of said chain;

each of said link plates having a concave bottom surface continuing from and defined between its opposed inside tooth faces at a position to avoid interference of said concave bottom surface with corresponding tooth edges of said sprocket teeth, which arises due to said polygonal motion when said outside tooth faces of said link plate are brought into meshing contact with said sprocket teeth and become seated thereon; and

said inside tooth faces having profiles identical to tooth profiles, arranged axially, of a hob cutter capable of forming said teeth of said sprocket; wherein the concave bottom surface of each of said link plates is an arc-shaped surface scooped out more deeply than an arc tangent to said opposed inside tooth faces.

2(Previously presented). A silent chain power transmission apparatus according to claim 1, wherein said V-shaped teeth have tooth edges profiled at a position where interference of said tooth edges with root bottoms defined between opposed ones of said teeth of said sprocket, which arises due to said polygonal motion when said outside tooth faces of said link plates are brought into meshing contact with said opposed ones of said sprocket teeth and become seated thereon, can be avoided.

3(Cancelled).